

# Music 206: Delay and Digital Filters I

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# Digital Filters

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- Any medium through which a signal passes may be regarded as a filter.
- Typically however, a filter is viewed as something which modifies the signal in some way. Examples include:
  - audio speakers / headphones
  - rooms / acoustic spaces
  - musical instruments
- A *digital* filter is a formula for going from one digital signal to another.

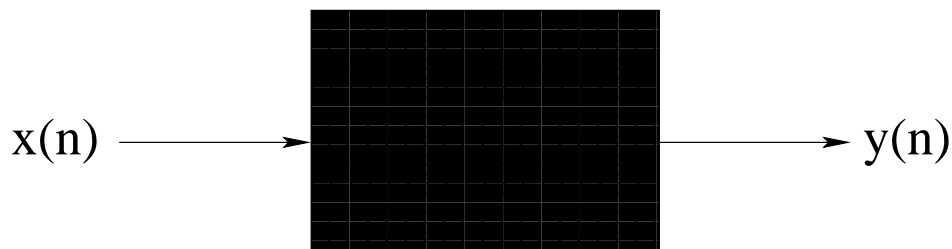


Figure 1: A black box filter.

# Inside the Black Box—Pure Delay

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- Time-domain implementations of digital filters involve signal *delay*, that is, *delayed* versions of input and/or output signals.
- What does it mean to delay an audio signal?
  - move it later (or earlier) in time
  - change the initial phase of signal, i.e., the value at time=0.

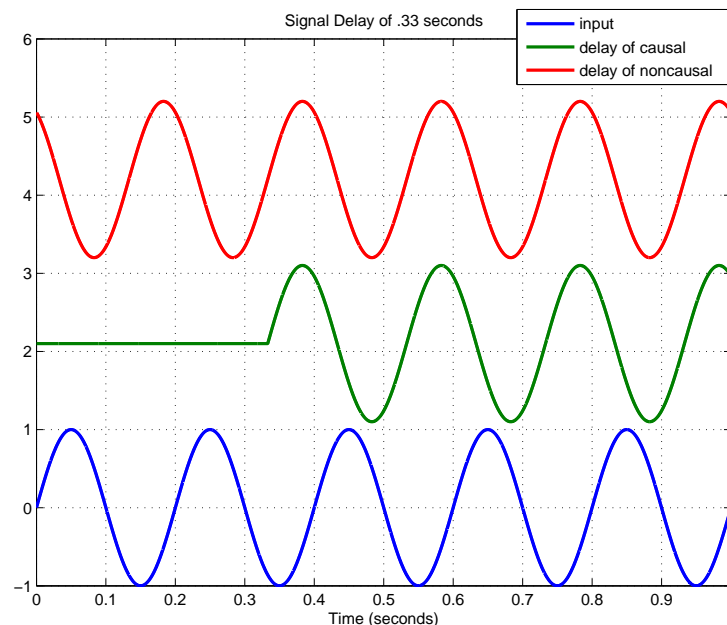


Figure 2: Timeshifting a signal will change the phase of the signal.

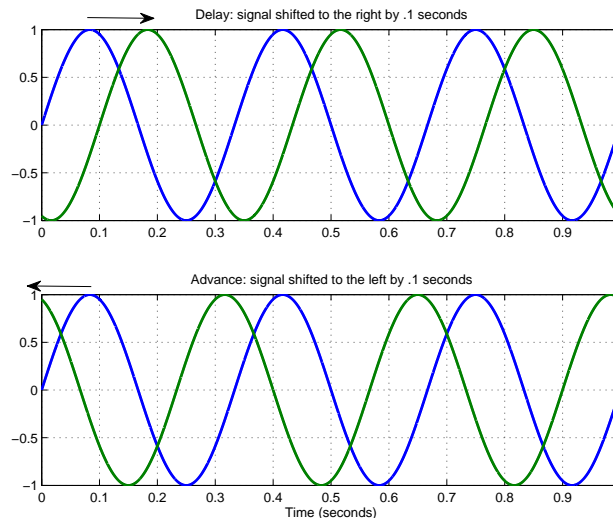
# Time shifting a signal

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- Whenever a signal can be expressed in the form

$$y(n) = x(n - M),$$

$y(n)$  is a *delayed* (time-shifted) version of  $x(n)$ .



- **If  $M$  is a positive number,**

$$y(n) = x(n - M),$$

the shift on the time axis is to the *right*.

- **If  $M$  is a negative number,**

$$y(n) = x(n + M),$$

the shift on the time axis is to the *left* (the signal has been advanced in time).

## Time shift and addition

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- Other than hearing a possible silence (for causal signals) before the signal onset, there is no audible effect of a *pure* delay.
- What happens, however, when a signal  $x(n)$  is added to a delayed version of itself  $x(n - M)$ ?
- We have created a *digital filter*, with a formula for going from input  $x(n)$  to output  $y(n)$  given by the difference equation

$$y(n) = x(n) + x(n - M).$$

# A Running Averager

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- In a simple case where  $M = 1$ ,

$$y(n) = x(n) + x(n - 1),$$

we are taking a *running average* of the input signal  $x(n)$ .

This filter takes the average of two adjacent samples (with a gain of 2).
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# Intuitive Analysis at Low Frequencies

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- The running average of a signal with little or no variation from sample to sample will be very close to the input signal.
- At DC

$$x_1(n) = [A, A, A, \dots].$$

- The output of the filter is

$$\begin{aligned} y(n) &= x_1(n) + x_1(n-1) \\ &= [A, A, A, \dots] \\ &\quad + [0, A, A, A, \dots] \\ &= [A, 2A, 2A, 2A, \dots] \end{aligned}$$

The output is effectively the same as the input, but with a gain of 2.

# Intuitive Analysis at High Frequencies

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- The running average of an input signal with significant variation from sample to sample will be very different from its input.
- At  $f_s/2$  (Nyquist limit)

$$x_2(n) = [A, -A, A, \dots].$$

- The output of the filter is

$$\begin{aligned} y(n) &= x_2(n) + x_2(n-1) \\ &= [A, -A, A, \dots] \\ &\quad + [0, A, -A, A, \dots] \\ &= [A, 0, 0, 0, \dots] \end{aligned}$$

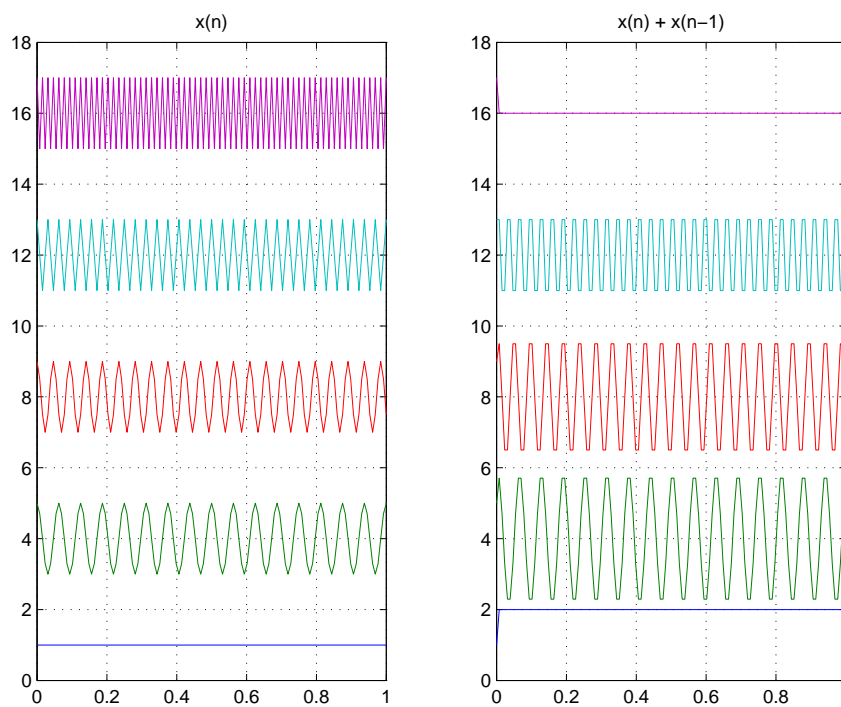
The output is different from the input—complete attenuation.



## What about all the frequencies in between?

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- We may find the frequency response of the filter by checking the behaviour of the filter at every possible frequency between 0 and  $f_s/2$  Hz (sinewave analysis).



- This filter boosts low frequencies while attenuating higher frequencies—it is a *lowpass* filter.

# Impulse Response

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- Alternatively, we can use an input signal that contains all frequency components, and then we only have to do the “checking” operation once.
- An input signal with the broadest possible spectrum would be an *impulse*.
- The response of a filter to an impulse is called an *impulse response*.

Any filter in a large class known as linear, time-invariant (LTI), is completely characterized by its impulse response.

- What is the impulse response of this filter?

# Frequency Response

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- The spectrum of the impulse response gives us the *frequency response* from which we may see how the filter modifies the *amplitude* and *phase* of a signal's sinusoidal components.

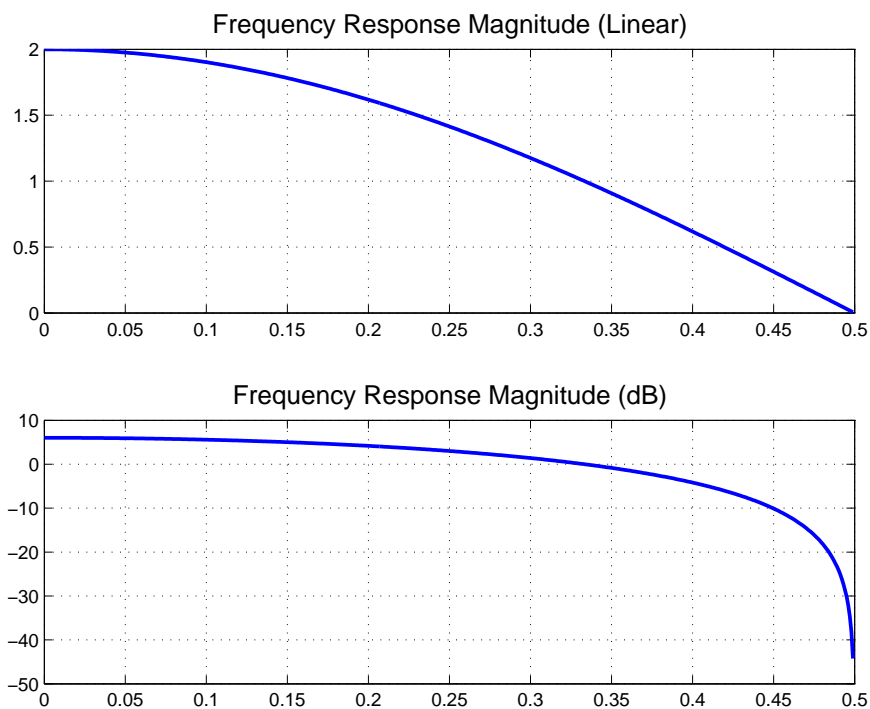


Figure 3: Magnitude of the Frequency Response shows a low-pass characteristic.

# Response at the Cutoff Frequency

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- Look a little closer at the filter's response to  $f_s/4$ .

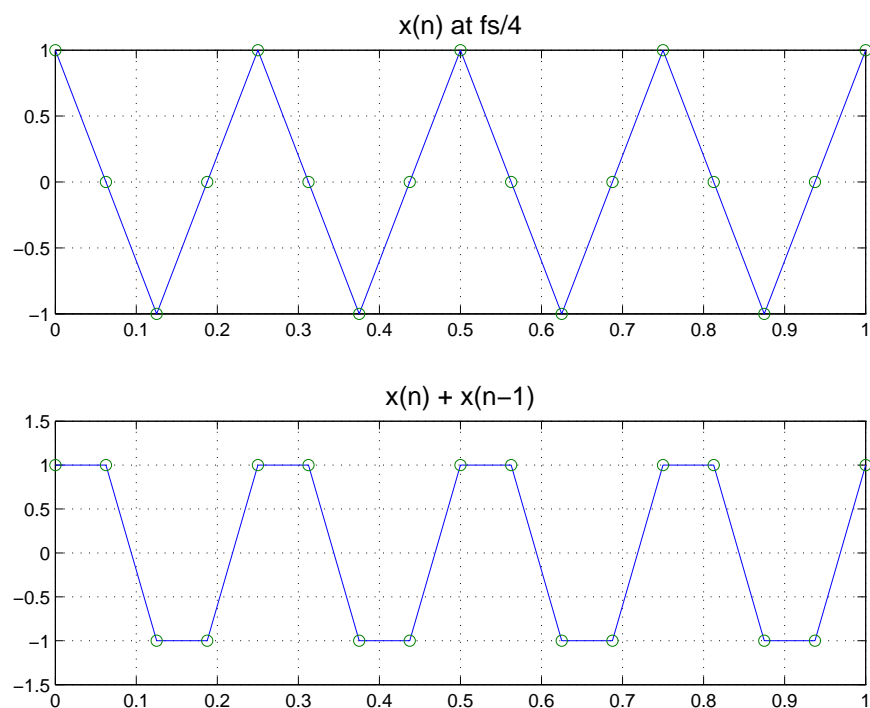


Figure 4: Filter behaviour at  $f_s/4$ .

# Interpreting the Phase

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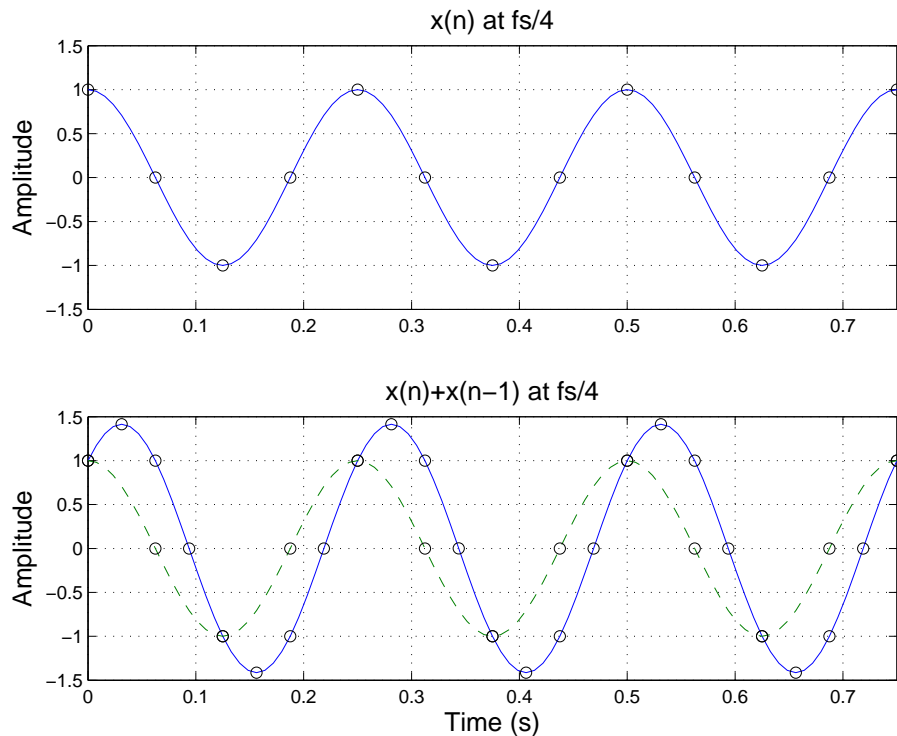


Figure 5: Filter behaviour at  $f_s/4$ .

- This filter is *delaying* this frequency by half a sample.
- In fact, this filter delays *all* frequencies by half a sample.

# Linear Phase Filters

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- Filters that delay all frequencies by the same amount are called *linear phase* filters.
- Linear phase filters have a symmetric impulse response.

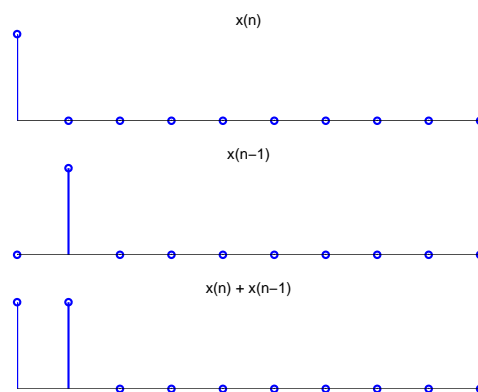


Figure 6: Filter impulse response.

- For this filter, the impulse response is symmetric about sample 0.5, which corresponds to a waveform delay of one-half sample at all frequencies.

# Phase Delay

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- The value about which the impulse response is symmetric is the *phase delay* of the filter.

A “simple waveform delay” means the waveform will not change with a change in frequency.

- Linear phase is desirable because it delays all frequencies by the same number of samples and that means **no phase distortion**.

# Changing Filter Coefficients

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- Consider the following variation on the two-point averager (lowpass filter):

$$y(n) = x(n) - x(n - 1).$$

How does changing the addition to a subtraction change the filter?

Changing the addition to a subtraction changes the *coefficients* of the filter.

- At DC the output becomes

$$\begin{aligned} y(n) &= x_1(n) - x_1(n - 1) \\ &= [A, A, A, \dots] \\ &\quad - [0, A, A, A, \dots] \\ &= [A, 0, 0, 0, \dots] \end{aligned}$$

- At the Nyquist limit the output becomes

$$\begin{aligned} y(n) &= x_2(n) - x_2(n - 1) \\ &= [A, -A, A, \dots] \\ &\quad - [0, A, -A, A, \dots] \\ &= [A, -2A, 2A, -2A, \dots] \end{aligned}$$



## Notch and Bandpass Filters

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- Consider next, changing the delay value of the second term:

$$y(n) = x(n) + x(n - 2).$$

- This changes the filter order to 2 and effectively sets the  $x(n - 1)$  term to zero.

The filter *order* is the value of its highest delay.

- This filter passes both DC and the Nyquist limit, but attenuates  $f_s/4$ . It is a notch filter.
- The filter given by

$$y(n) = x(n) - x(n - 2)$$

rejects DC and the Nyquist limit, and boosts  $f_s/4$ . It is a bandpass filter.

# Plots of simple filters

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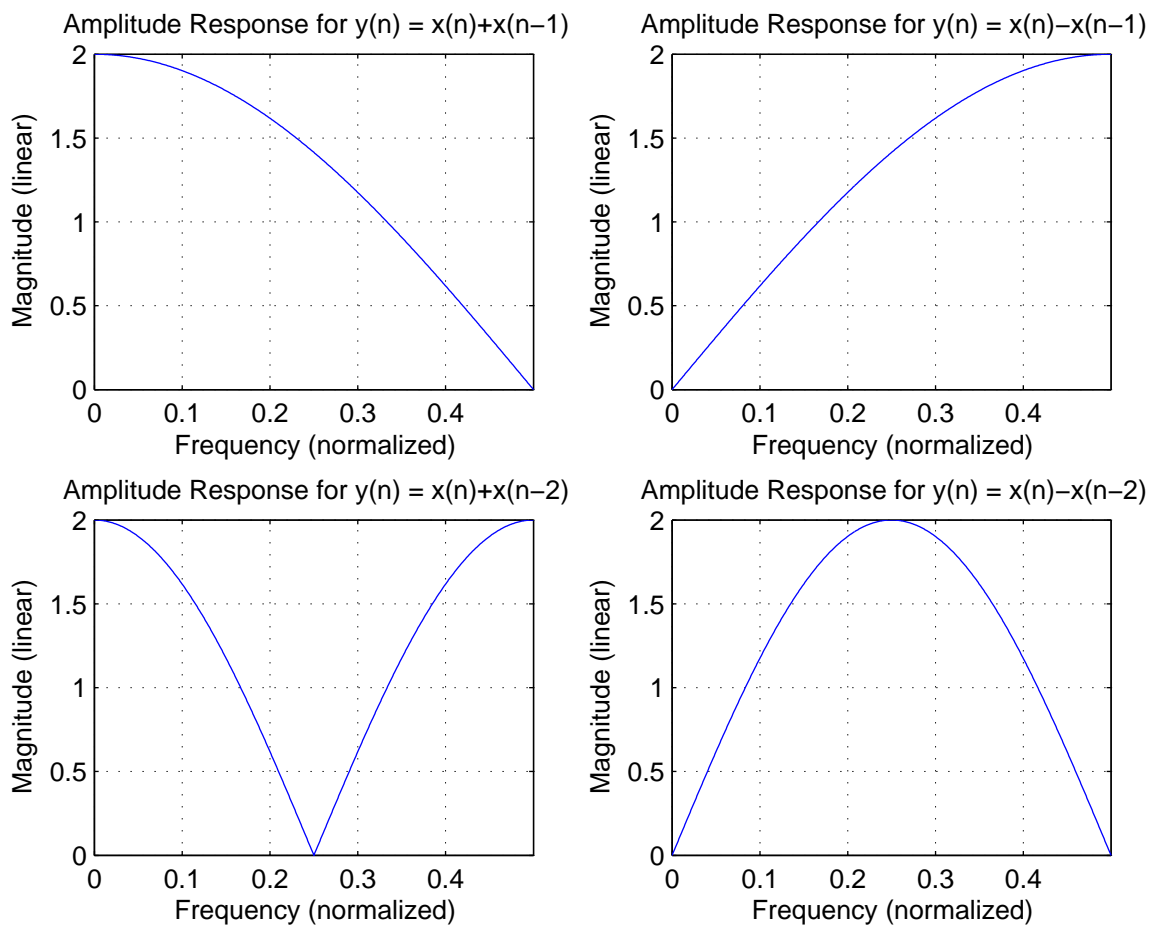


Figure 7: Amplitude Responses for simple filters

# Increasing the Filter Order

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- Let's return now to the simple low-pass filter

$$y(n) = x(n) + x(n - 1)$$

- Increasing the order will increase the number of samples averaged

$$y(n) = x(n) + x(n - 1) + x(n - 2),$$

and the waveform will be smoothed (with a more gentle slope to zero) which corresponds to a lowered cutoff frequency

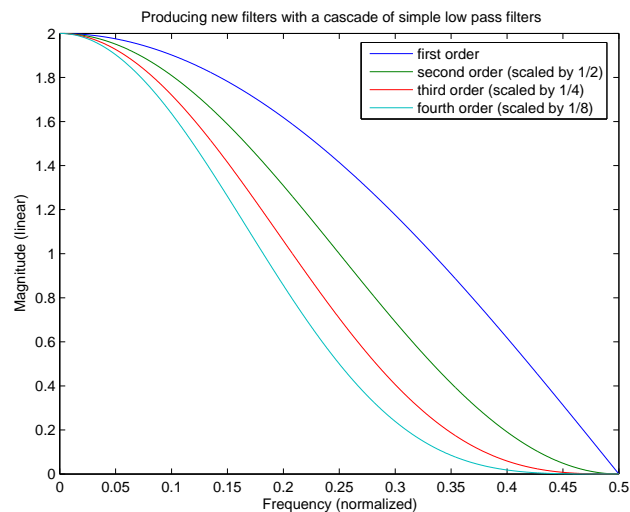


Figure 8: Lowpass filters of increasing order.

## Generalized FIR filter

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- Several different (nonrecursive) filters can be made by changing the delay and the coefficients of the filter terms,

$$y(n) = b_0x(n) + b_1x(n - 1) + \dots \\ b_2x(n - 2) + \dots + b_Mx(n - M),$$

where  $M$  is the maximum delay and thus the order of the filter.

- A filter can be defined simply by a set of coefficients. For example if

$$b_k = \{1, 3, 3, 1\},$$

the filter is third order (has a maximum delay of  $M = 3$ ), and can be expanded into the difference equation

$$y(n) = x(n) + 3x(n - 1) + 3x(n - 2) + x(n - 3)$$

## Coefficients as Impulse Response

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- The impulse response  $y(n) = h(n)$  is equivalent to coefficients of our FIR filter  $b_k$ .
- This can be shown using the general FIR equation, with input  $x(n) = \delta(n)$  (recall  $\delta$  only has a nonzero value when  $n = 0$ ).

$$\begin{aligned} h(0) &= b_0\delta(0) + b_1\delta(0-1) + b_2\delta(0-2) + \dots \\ &= b_0, \end{aligned}$$

$$\begin{aligned} h(1) &= b_0\delta(1) + b_1\delta(1-1) + b_2\delta(1-2) + \dots \\ &= b_1, \end{aligned}$$

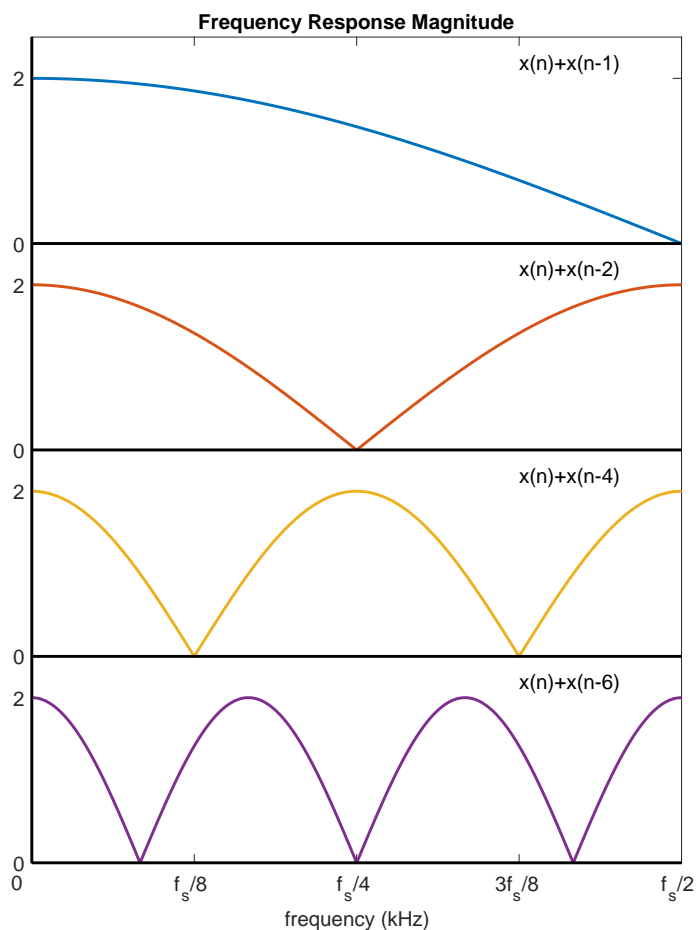
$$\begin{aligned} h(2) &= b_0\delta(2) + b_1\delta(2-1) + b_2\delta(2-2) + \dots \\ &= b_2, \end{aligned}$$

...

- When the relation between the input  $x(n)$  and the output  $y(n)$  of the FIR filter is expressed in terms of the input and impulse response, we say the output is obtained by *convolving* the sequences  $x(n)$  and  $h(n)$ .

## Increasing the phase delay

- Again returning to the simple low pass filter...
- What happens when the delay is increased?



- Notice appearance of regularly spaced peaks/notches (like teeth of a “comb”).

# The Feedforward Comb Filter

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- Increasing the delay of the “simple” first-order lowpass filter

$$y(n) = x(n) + gx(n - M),$$

where  $g$  is the coefficient multiplying the delay, calls for use of a delay line:

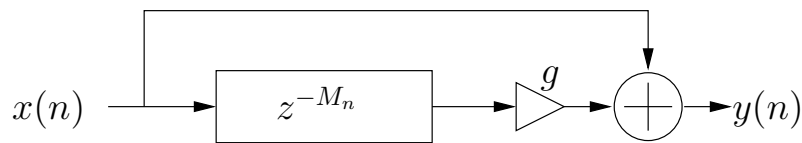


Figure 9: A feedforward comb filter.

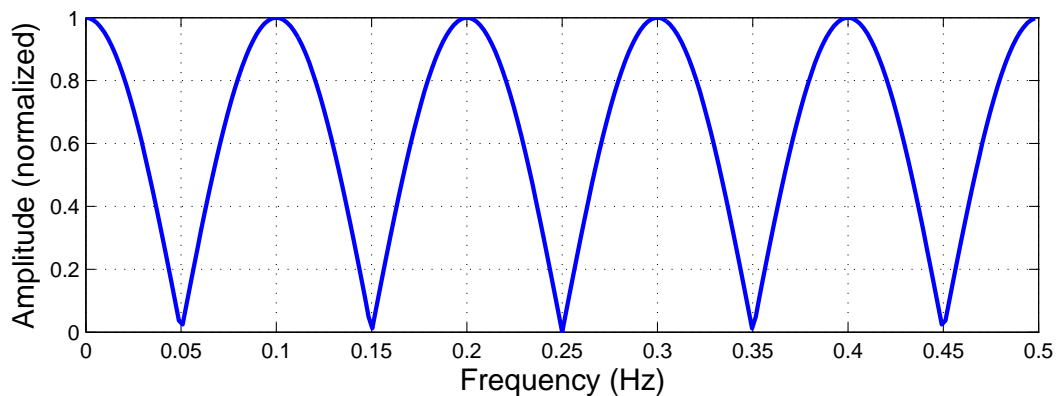


Figure 10: The comb filter magnitude response.

# The Delay Line

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- The **delay line** is an elementary functional unit modeling *acoustic propagation delay* (e.g. digital waveguide models and delay effects processors).

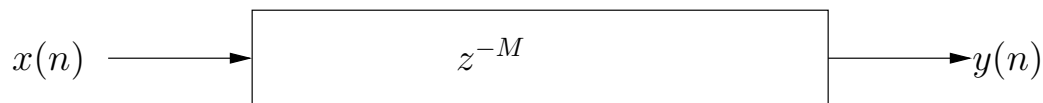


Figure 11: The  $M$ -sample delay line.

- The delay line introduces a time delay (phase delay of  $M$  samples) between input  $x(n)$  and output  $y(n)$ :

$$y(n) = x(n - M), \quad n = 0, 1, 2, \dots$$

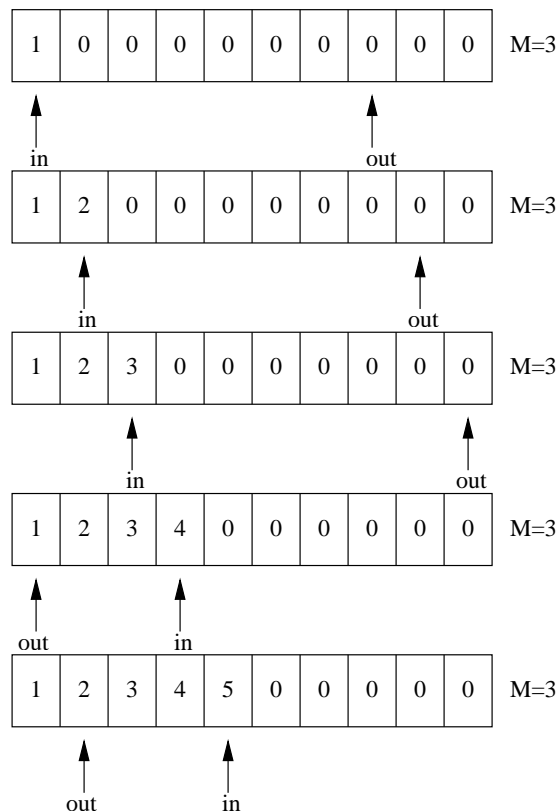
- It is linear phase (delay is the same at all frequencies) as can be seen by the **symmetry of the impulse response** about the  $M^{\text{th}}$  sample.



# Circular Delay Line

- If  $M$  changes over time, delay may be implemented using write (in) and read (out) pointers into a larger buffer.
- The delay is set by having the read (out) pointer “chase” the write (in) pointer by the desired delay.

**input sequence:** 1, 2, 3, 4, 5, etc.



**output sequence:** 0, 0, 0, 1, 2, 3, 4, etc.

## Practical Example

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- If the wave propagates  $L = 1$  meter:

- Sampling rate:

$$f_s = 44100$$

- Temporal sampling period:

$$T = \frac{1}{44100}$$

- Spatial sampling period (distance traveled in one sample assuming propagation speed of 340 m/s):

$$X = cT = \frac{340}{44100} = 7.7\text{mm}$$

- Number of samples delay:

$$M = \frac{L}{X} = \frac{1}{cT} = \frac{1}{0.0077} = 130$$

# The Delay Line Coefficient $g$

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- The feedforward coefficient  $g$  controls the proportion of the delay signal in the output.

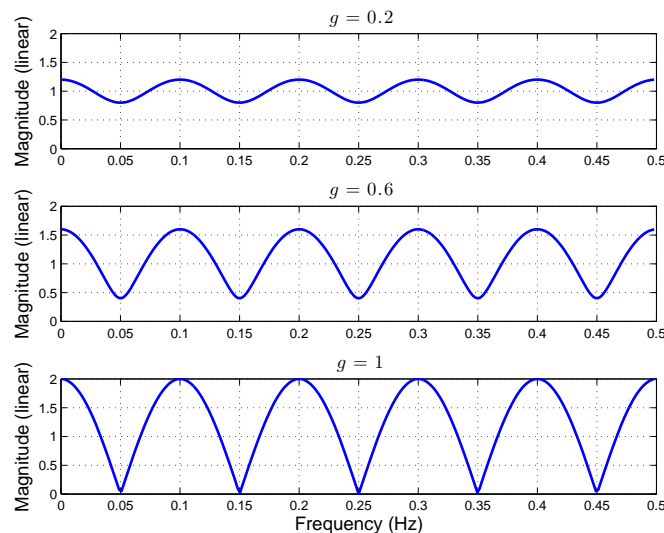


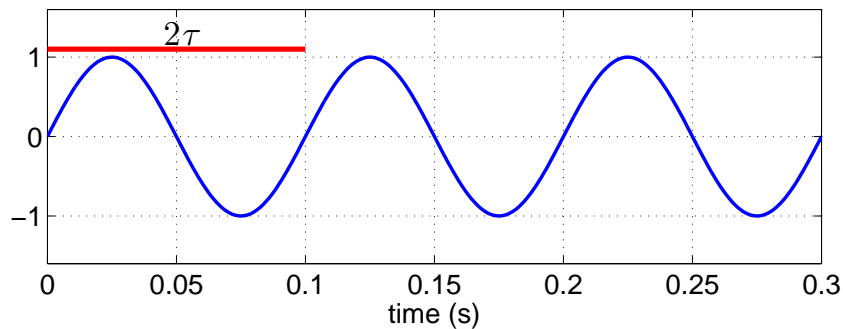
Figure 12: Delayline coefficient controls notch attenuation and peak gain.

- It can be viewed as the DEPTH parameter, setting
  - the amount of **gain** at the maxima,
  - the amount of **attenuation** at the minima,that is, the *depth* from the peaks to the notches.
- Has a range from 0 to 1 (1 corresponds to maximum depth).

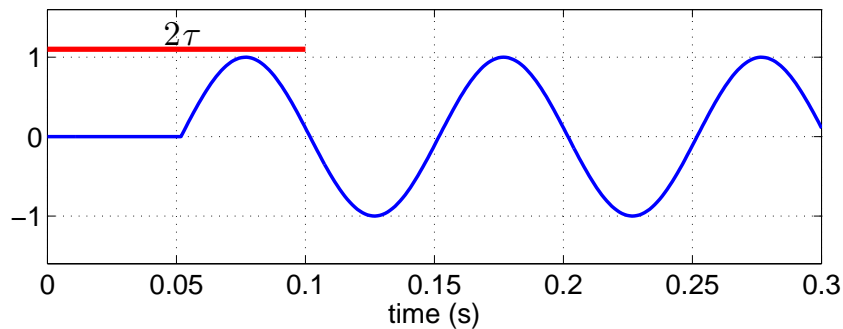
# Cancellation at Notch Frequencies

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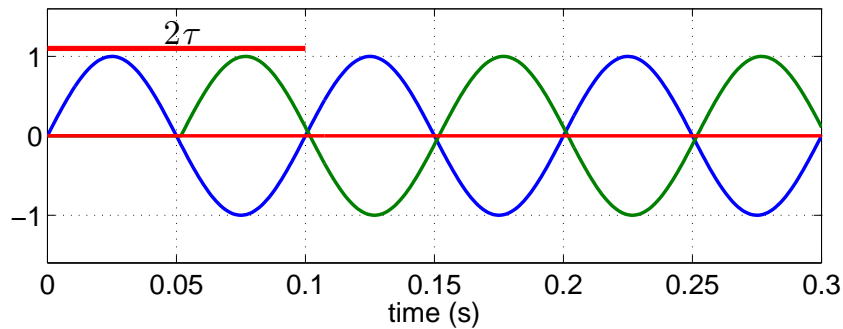
- Consider a sinusoid at  $f = 1/(2\tau)$  (period of  $2\tau$ ):



- Delaying that sinusoid by  $\tau$  ( $1/2$  a period) yields:



- Summing with original yields complete cancellation:



## Relating $\tau$ to delay of $M$ samples

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- For  $y(n) = x(n) + x(n - M)$  delay is  $M$  samples or

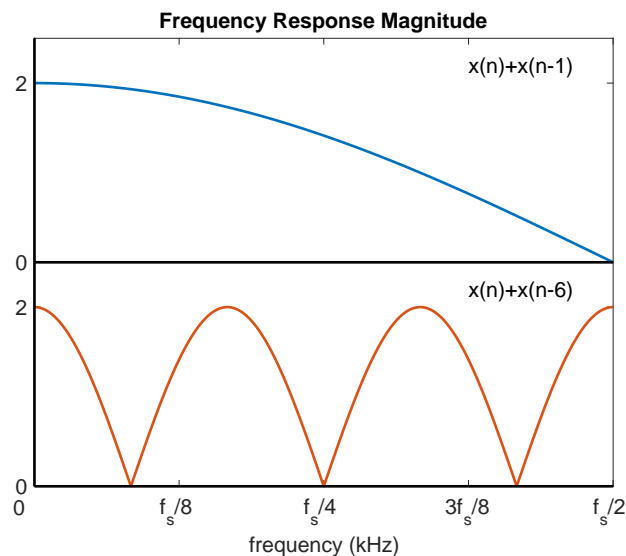
$$\tau = \frac{M}{f_s} \text{ seconds.}$$

- There is complete attenuation (notch) at frequency

$$f = \frac{1}{2\tau} = \frac{1}{2M/f_s} = \frac{f_s}{2M}$$

and at odd harmonics  $3f, 5f, \dots$  (up to Nyquist limit).

- For  $M = 1$  (lowpass) there is 1 notch at  $f_s/2$ .



- For  $M = 6$  there are notches at  $f_s/12, f_s/4, 5f_s/12$ .

# Why Spectral Notches?

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- Notches occur in the spectrum as a result of **destructive interference**.
- Recall that delaying a sine tone 180 degrees (1/2 a cycle) and summing with the original will cause the signal to disappear at the output.

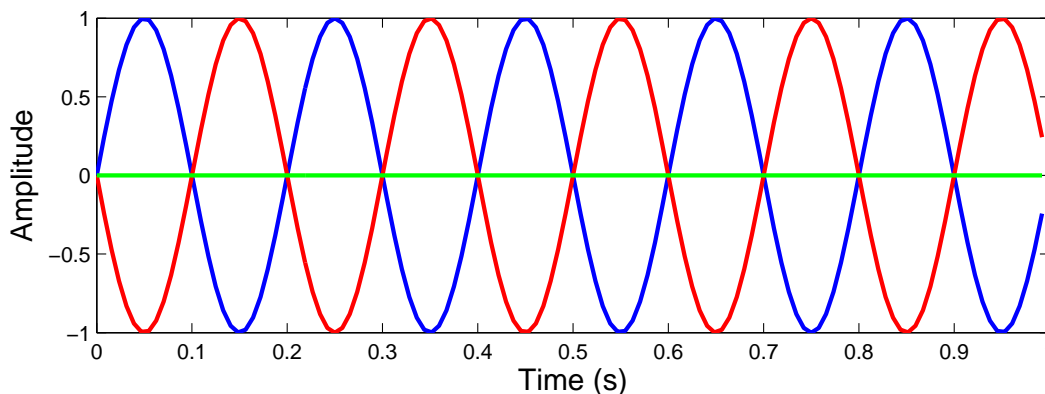


Figure 13: Complete destructive interference.

- If a sinusoid has a frequency of  $f_0$ , then a delay of 1/2 cycle corresponds to a delay of

$$\tau = \frac{1}{2f_0} \text{ seconds}$$

or

$$M = \frac{f_s}{2f_0} \text{ samples.}$$

## Delay Parameter $M$

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- A delay of  $M = f_s/(2f_0)$  samples in the comb filter will yield a *notch* (complete cancelation) at

$$f_0 = \frac{f_s}{2M} \text{ Hz,}$$

as well as notches at **odd harmonics** of  $f_0$ .

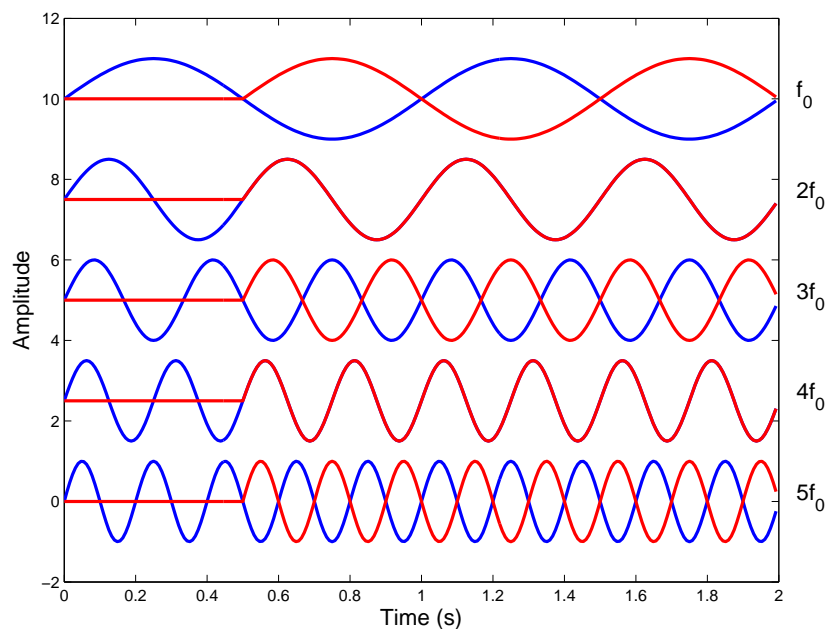


Figure 14: Destructive interference occurs at odd harmonics of the fundamental frequency.

- The well known *flanger* is a feedforward comb filter with a time-varying delay  $M(n)$  (see flanging.mov).