

The Role of Lip Reflection/Transmission in the Relationship Between LPC and Waveguide Vocal Tract Models

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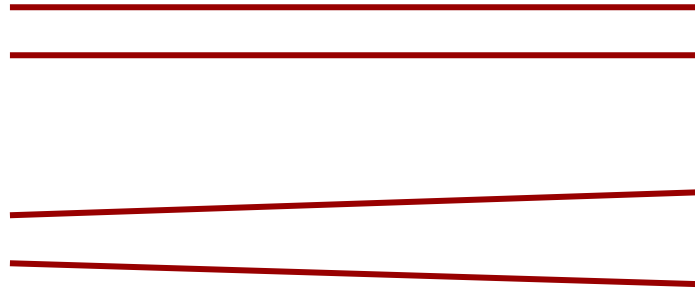
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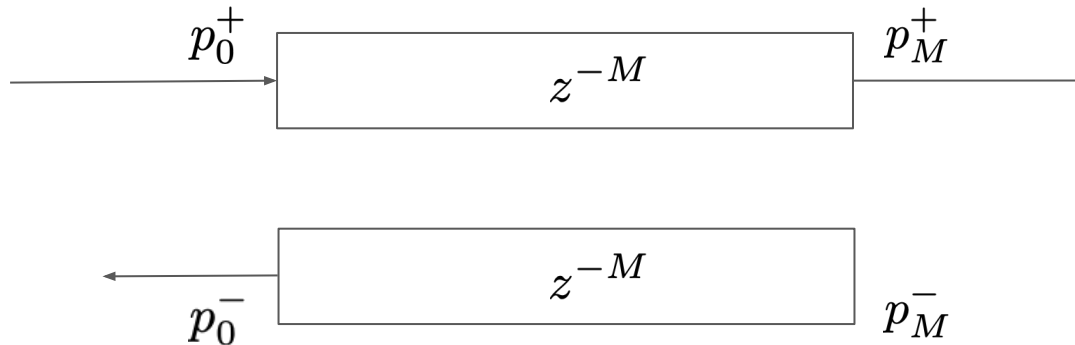
Summary

- Piecewise cylindrical waveguide model (Kelly-Lochbaum) of the vocal tract (acoustic tubes having varying cross-sectional area).
 - matrix representation leading to **three (3) transfer function**:
 - 1. non-polynomial form (sufficient for frequency-domain implementation)
 - 2. polynomial in z , with **scalar** loss
 - 3. polynomial in z , with **frequency-dependent** loss
 - acoustically-informed cylindrical open-end reflection function at the lips (shelf filter)
 - relationship to LPC
 - estimation of loss coefficients from LPC coefficients

Cylindrical and Conical Acoustic Tubes

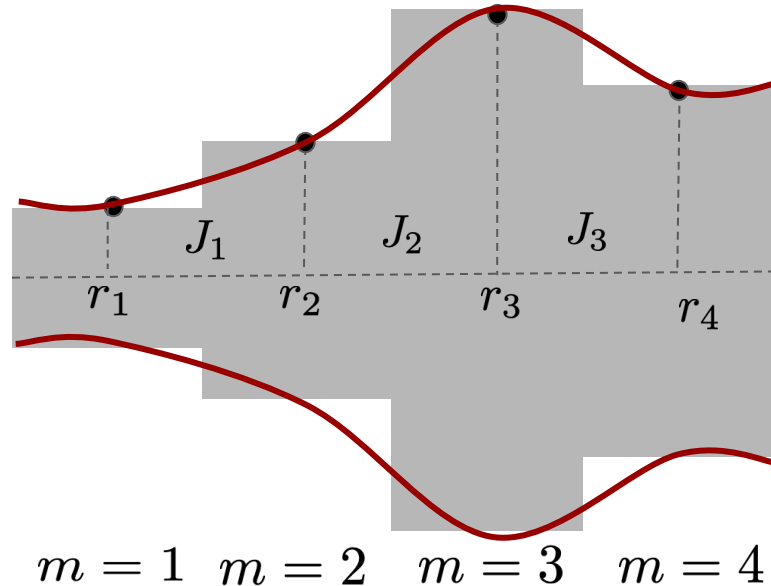


Waveguide Section

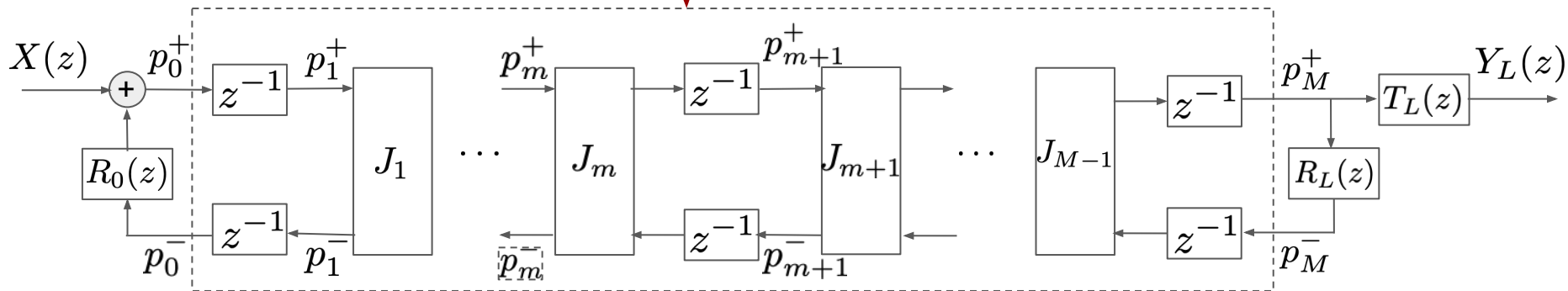
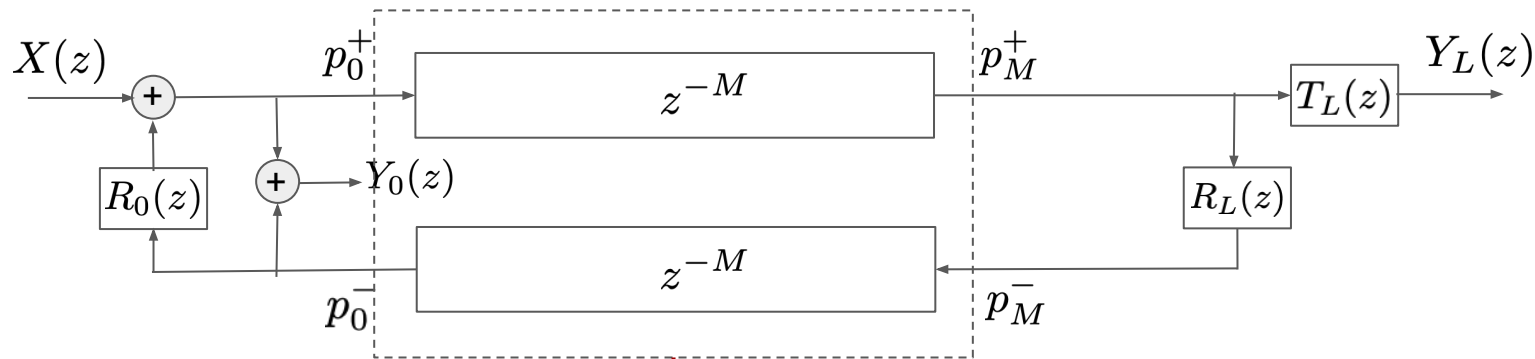


Acoustic Tube with Varying Cross-Sectional Area

Radii sampled/measured at regular spatial intervals
allows for a piecewise approximation

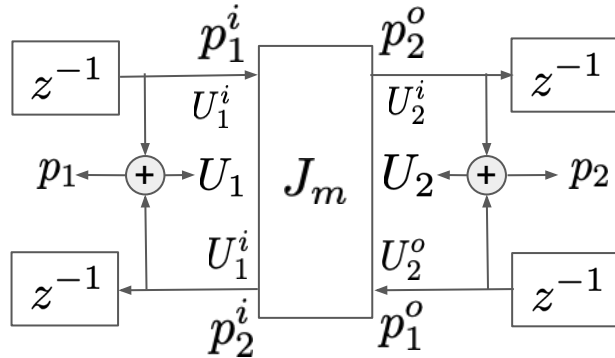


Piecewise Waveguide Model



Two-port scattering junction and port input/output (I/O)

The law for conservation of mass and momentum:



- pressure** at junction equals pressure on each port

$$p_J = p_1 = p_2 \longrightarrow p_1^i + p_1^o = p_2^i + p_2^o$$

- volume velocity** on the each port sums to zeros

$$U_1 + U_2 = 0 \longrightarrow U_1^i + U_1^o = -(U_2^i + U_2^o)$$

Characteristic impedance (cylinders) : $Z_n = \frac{\rho c}{S_n}$
 cross-sectional area

$$U_n^i = \frac{p_n^i}{Z_n} \quad U_n^o = -\frac{p_n^o}{Z_n}$$

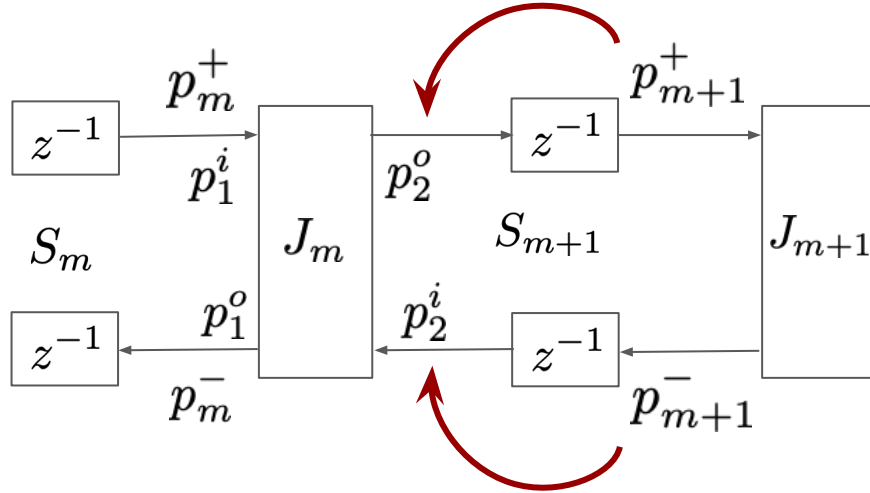
Matrix representation:

$$\mathbf{C} \begin{bmatrix} p_1^i \\ p_1^o \end{bmatrix} = \mathbf{D} \begin{bmatrix} p_2^i \\ p_2^o \end{bmatrix}$$

$$\mathbf{C} = \begin{bmatrix} 1 & 1 \\ S_1 & -S_1 \end{bmatrix}$$

$$\mathbf{D} = \begin{bmatrix} 1 & 1 \\ -S_2 & S_2 \end{bmatrix}$$

Port I/O and Right/Left Traveling Waves



$$\mathbf{C} \begin{bmatrix} p_1^i \\ p_1^o \end{bmatrix} = \mathbf{D} \begin{bmatrix} p_2^i \\ p_2^o \end{bmatrix}$$

$$\underbrace{\begin{bmatrix} p_1^i \\ p_1^o \end{bmatrix}}_{\mathbf{p}_m} = \underbrace{\mathbf{C}^{-1}\mathbf{D}}_{(\mathbf{C}^{-1}\mathbf{D})_m} \underbrace{\begin{bmatrix} p_2^i \\ p_2^o \end{bmatrix}}_{\begin{bmatrix} p_{m+1}^- z^{-1} \\ p_{m+1}^+ z \end{bmatrix}}$$

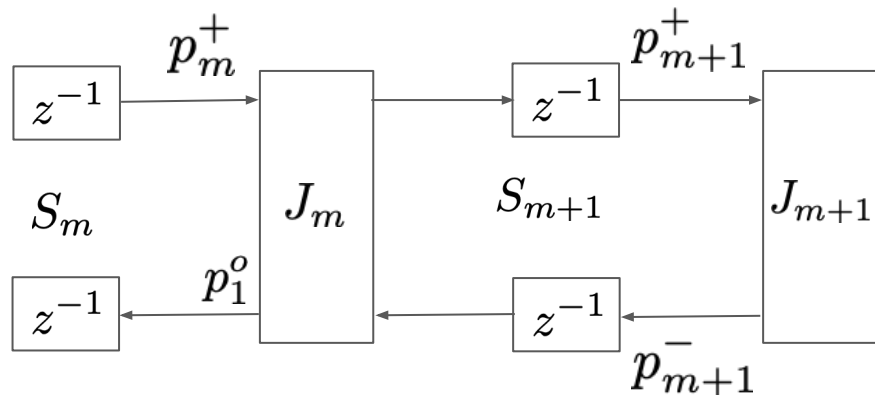
$$\mathbf{C}^{-1}\mathbf{D} = \frac{1}{2S_1} \begin{bmatrix} S_1 - S_2 & S_1 + S_2 \\ S_1 + S_2 & S_1 - S_2 \end{bmatrix}$$

$$\begin{bmatrix} 0 & z^{-1} \\ z & 0 \end{bmatrix} \underbrace{\begin{bmatrix} p_{m+1}^+ \\ p_{m+1}^- \end{bmatrix}}_{\mathbf{p}_{m+1}}$$

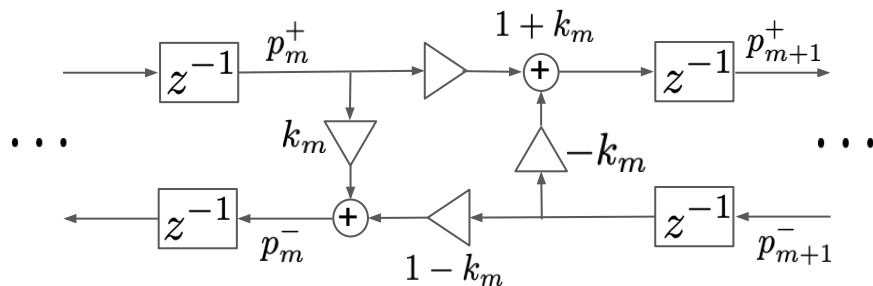
$$\mathbf{C}^{-1}\mathbf{D} = \frac{1}{2S_1} \begin{bmatrix} S_1 - S_2 & S_1 + S_2 \\ S_1 + S_2 & S_1 - S_2 \end{bmatrix}$$

$$(\mathbf{C}^{-1}\mathbf{D})_m = \frac{1}{2S_m} \begin{bmatrix} S_m - S_{m+1} & S_m + S_{m+1} \\ S_m + S_{m+1} & S_m - S_{m+1} \end{bmatrix}$$

Scattering Matrix and Reflection Coefficients



Kelly-Lochbaum Scattering Junction



$$\underbrace{\begin{bmatrix} p_m^+ \\ p_m^- \end{bmatrix}}_{\mathbf{p}_m} = \underbrace{(\mathbf{C}^{-1}\mathbf{D})_m}_{\mathbf{A}_m} \underbrace{\begin{bmatrix} 0 & z^{-1} \\ z & 0 \end{bmatrix}}_{\mathbf{A}_m} \underbrace{\begin{bmatrix} p_{m+1}^+ \\ p_{m+1}^- \end{bmatrix}}_{\mathbf{p}_{m+1}}$$

Scattering matrix:

$$\begin{aligned} \mathbf{A}_m &= \frac{1}{2S_m} \begin{bmatrix} S_m - S_{m+1} & S_m + S_{m+1} \\ S_m + S_{m+1} & S_m - S_{m+1} \end{bmatrix} \begin{bmatrix} 0 & z^{-1} \\ z & 0 \end{bmatrix} \\ &= \frac{z}{1 + k_m} \begin{bmatrix} 1 & k_m z^{-2} \\ k_m & z^{-2} \end{bmatrix} \end{aligned}$$

where $k_m = \frac{S_m - S_{m+1}}{S_m + S_{m+1}}$ (reflection coefficients)

“Chain” Scattering Matrix

Relationship between traveling waves in adjacent sections:

$$\mathbf{p}_m = \mathbf{A}_m \underbrace{\mathbf{p}_{m+1}}_{\mathbf{A}_{m+1} \underbrace{\mathbf{p}_{m+2}}_{\mathbf{A}_{m+2} \mathbf{p}_{m+3}}}$$

scattering matrix:

$$\mathbf{A}_m = \frac{z}{1 + k_m} \begin{bmatrix} 1 & k_m z^{-2} \\ k_m & z^{-2} \end{bmatrix}$$

... and between first and final sections:

$$\mathbf{p}_1 = \left(\prod_{m=1}^{M-1} \mathbf{A}_m \right) \mathbf{p}_M$$

$$\prod_{m=1}^N \mathbf{A}_m = \frac{z}{1 + k_1} \begin{bmatrix} 1 & k_1 z^{-2} \\ k_1 & z^{-2} \end{bmatrix} \frac{z}{1 + k_2} \begin{bmatrix} 1 & k_2 z^{-2} \\ k_2 & z^{-2} \end{bmatrix} \cdots \frac{z}{1 + k_N} \begin{bmatrix} 1 & k_N z^{-2} \\ k_N & z^{-2} \end{bmatrix} \quad \begin{array}{l} \text{number of junctions:} \\ N = M - 1 \end{array}$$

$$\begin{array}{l} \text{pure delay} \left\{ \begin{array}{l} z^N \\ \prod_{m=1}^N (1 + k_m) \end{array} \right\} \\ \text{gain} \left\{ \right. \end{array} \frac{z^N}{\prod_{m=1}^N (1 + k_m)} \mathbf{K}_N$$

“chain” scattering matrix:

$$\mathbf{K}_N = \prod_{m=1}^N \begin{bmatrix} 1 & k_m z^{-2} \\ k_m & z^{-2} \end{bmatrix} = \begin{bmatrix} K_{1,1} & K_{1,2} \\ K_{2,1} & K_{2,2} \end{bmatrix}$$

Matrix Entries and Polynomial Coefficients

“Chain” Scattering Matrix:

$$\mathbf{K}_N = \prod_{m=1}^N \begin{bmatrix} 1 & k_m z^{-2} \\ k_m & z^{-2} \end{bmatrix} = \begin{bmatrix} K_{1,1} & K_{1,2} \\ K_{2,1} & K_{2,2} \end{bmatrix} \quad \left. \vphantom{\prod_{m=1}^N} \right\}$$

Entries are polynomial in z :

$$\begin{aligned} K_{1,1} &= \sum_{m=0}^{N-1} c_{2m} z^{-2m} & K_{1,2} &= \sum_{m=1}^N d_{2(N-m)} z^{-2m} \\ K_{2,1} &= \sum_{m=0}^{N-1} d_{2m} z^{-2m} & K_{2,2} &= \sum_{m=1}^N c_{2(N-m)} z^{-2m} \end{aligned}$$

right column
coefficients
in reverse order

Initial coefficients: $c_0 = 1$ $d_0 = k_1$

Coefficients are recursively defined:

$$\mathbf{c}_N = \begin{bmatrix} \mathbf{c}_{N-1} \\ 0 \\ 0 \end{bmatrix} + k_N \begin{bmatrix} 0 \\ \tilde{\mathbf{d}}_{N-1} \\ 0 \end{bmatrix} \quad \mathbf{d}_N = \begin{bmatrix} \mathbf{d}_{N-1} \\ 0 \\ 0 \end{bmatrix} + k_N \begin{bmatrix} 0 \\ \tilde{\mathbf{c}}_{N-1} \\ 0 \end{bmatrix}$$

\sim denotes order of elements is reversed

Polynomial coefficient vectors have the form:

$$\mathbf{c}_N = \begin{bmatrix} c_0 \\ 0 \\ c_2 \\ 0 \\ \vdots \\ c_{2(N-1)} \\ 0 \end{bmatrix} \quad \mathbf{d}_N = \begin{bmatrix} d_0 \\ 0 \\ d_2 \\ 0 \\ \vdots \\ d_{2(N-1)} \\ 0 \end{bmatrix}$$

Transfer Function 1: non-polynomial form

The transfer function is the (spectral) ratio of the model **output** to the **input**:

$$H_L(z) = \frac{Y_L(z)}{X(z)} = \frac{T_L(z)p_M^+}{p_1^+z - R_0p_1^-z^{-1}}$$

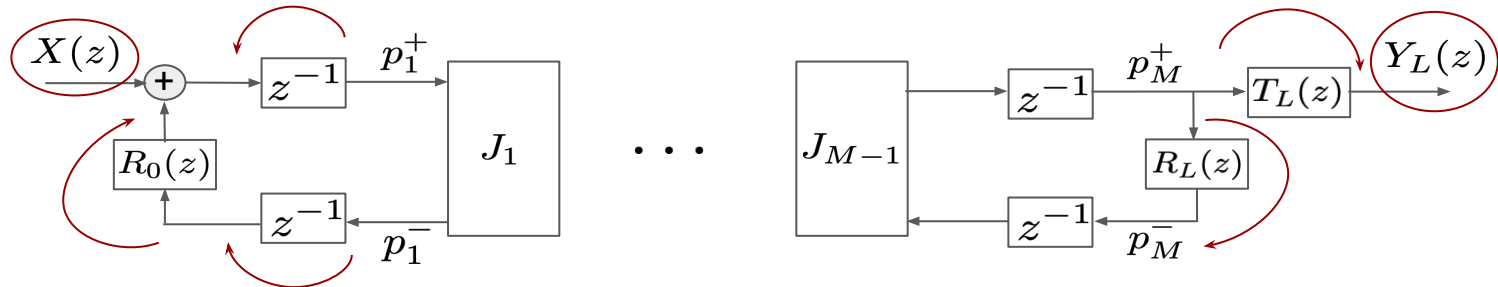
$$= \frac{T_L(z)z^{-(N+1)} \prod_{m=1}^N (1 + k_m)}{K_{1,1} + K_{1,2}R_L(z) - R_0 (K_{2,1} + K_{2,2}R_L(z)) z^{-2}}$$

Represent **first-section wave components** as a function of the **right-going component in the last section** using:

1. “chain” scattering matrix:

$$\mathbf{p}_1 = \frac{z^N}{\prod_{m=1}^N (1 + k_m)} \mathbf{K}_N \mathbf{p}_M$$

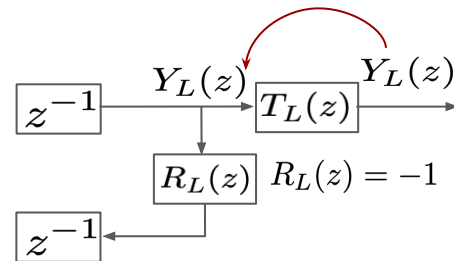
2. by definition: $p_M^- = p_M^+ R_L(z)$



Transfer Function 2: polynomial in z , scalar boundaries

$$H_L(z) = \frac{Y_L(z)}{X(z)} = \frac{T_L(z) z^{-(N+1)} \prod_{m=1}^N (1 + k_m)}{\underbrace{K_{1,1} + K_{1,2} R_L(z) - R_0 (K_{2,1} + K_{2,2} R_L(z))}_{\text{lumped scalar loss}} z^{-2}} = \frac{B(z)}{A(z)}$$

$$A(z) = a_0 z^{-0} + a_1 z^{-1} + \dots + a_{2(N+1)} z^{-2(N+1)}$$



Coefficient (column) vector:

$$\mathbf{A}_N = \begin{bmatrix} \mathbf{c}_N & 0 & 0 & 0 \\ \cdot & \tilde{\mathbf{d}}_N & 0 & 0 \\ \cdot & \cdot & \mathbf{d}_N & 0 \\ \cdot & \cdot & \cdot & \tilde{\mathbf{c}}_N \\ 0 & \cdot & \cdot & \cdot \\ 0 & 0 & \cdot & \cdot \\ 0 & 0 & 0 & \cdot \end{bmatrix} \quad \mathbf{R} = \begin{bmatrix} \cancel{c_0} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ c_2 & d_{2(N-1)} & d_0 & 0 \\ 0 & 0 & 0 & 0 \\ c_4 & d_{2(N-2)} & d_2 & c_{2(N-1)} \\ 0 & 0 & 0 & 0 \\ \vdots & \vdots & \vdots & \vdots \\ c_{2(N-1)} & d_2 & d_{2(N-2)} & c_4 \\ 0 & 0 & 0 & 0 \\ 0 & d_0 & d_{2(N-1)} & c_2 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & \cancel{c_0} 1 \end{bmatrix}$$

$$\mathbf{R} = \begin{bmatrix} 1 & \cancel{R_L} & -1 & \cancel{R_0} \\ & & & \end{bmatrix}^T$$

$$\mathbf{A}_N = \begin{bmatrix} 1 \\ 0 \\ a_2 \\ \vdots \\ 0 \\ a_{2N} \\ 0 \\ R_0 \end{bmatrix}$$

Relationship to LPC: impulse response of $H_L(z)$

Transfer Function:

$$H_L(z) = \frac{Y_L(z)}{X(z)} = \frac{z^{-(N+1)} \prod_{m=1}^N (1 + k_m)}{1 + \sum_{i=1}^{2(N+1)} \underbrace{a_i}_{\text{defined by } \mathbf{A}_N} z^{-i}}$$

Difference Equation:

$$y(n) = \prod_{m=1}^N (1 + k_m) \underbrace{x(n - (N + 1))} - \sum_{i=1}^{2(N+1)} a_i y(n - i)$$

Input impulse:

$$x(n) = u(n) = 1, 0, 0, 0, \dots$$

Impulse Response:

$$y(n) = h(n) = \begin{cases} 0, & \text{for } n < N + 1 \\ \prod_{m=1}^N (1 + k_m), & \text{for } n = N + 1 \\ - \sum_{i=1}^{2(N+1)} a_i h(n - i), & \text{for } n > N + 1. \end{cases}$$

Relationship to LPC: impulse response of $H_L(z)$

Impulse Response:

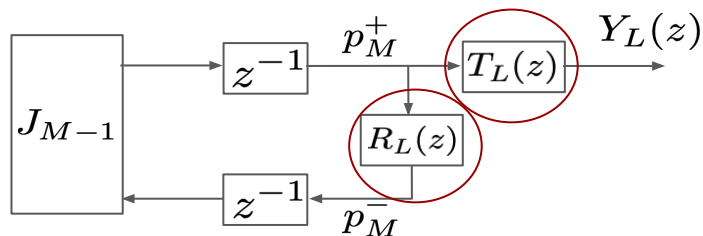
$$y(n) = h(n) = \begin{cases} 0, & \text{for } n < N + 1 \\ \prod_{m=1}^N (1 + k_m), & \text{for } n = N + 1 \\ - \sum_{i=1}^{2(N+1)} a_i h(n - i), & \text{for } n > N + 1. \end{cases}$$

Linear Prediction:

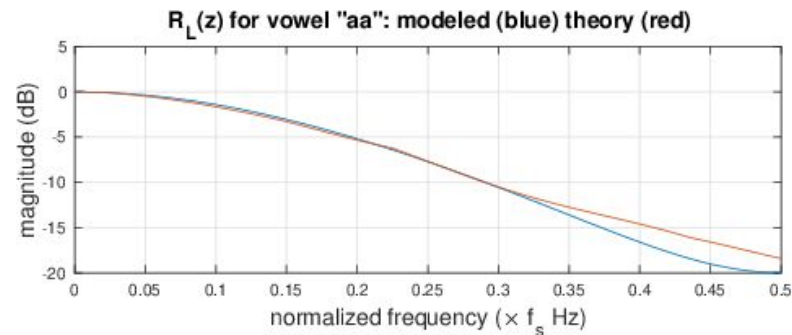
finds coefficients \hat{a}_i such that $\underbrace{\hat{x}(n)}_{\text{predicted signal}} = - \sum_{i=1}^{\overbrace{p}^{\text{order}}} \hat{a}_i x(n - i)$ error: $\cancel{e(n)} \overset{0}{=} x(n) - \hat{x}(n)$

If order $p = 2(N + 1)$ and $x(n) = h(n)$ then $\hat{x}(n) = h(n)$ and $\hat{a}_i = a_i$ $\mathbf{A}_N = \underbrace{\mathbf{A}_p}_{\text{LPC estimated coefficients vector}}$

Frequency-Dependent Lip Reflection



acoustically-informed reflection from an open cylinder:



Reflection function at the lips is made to be a **first-order shelf filter**:

$$R_L(z) = \frac{B_L(z)}{A_L(z)} = -\frac{(b_L)_0 + (b_L)_1 z^{-1}}{(a_L)_0 + (a_L)_1 z^{-1}} \quad \left. \vphantom{\frac{B_L(z)}{A_L(z)}} \right\} \text{coefficients are a function of the band-edge gain } g_\pi \text{ (see paper)}$$

When $0 < g_\pi < 1$, coefficients have the relationship: $(a_L)_0 - (b_L)_0 = -((a_L)_1 - (b_L)_1)$

Transmission function (amplitude complementary): $T_L(z) = 1 + R_L(z) = \frac{A_L(z) + B_L(z)}{A_L(z)}$.

Transfer Function 3: frequency-dependent lip reflection

Transfer function 1:

$$H_L(z) = \frac{Y_L(z)}{X(z)} = \frac{T_L(z) z^{-(N+1)} \prod_{m=1}^N (1 + k_m)}{K_{1,1} + K_{1,2} R_L(z) - R_0 (K_{2,1} + K_{2,2} R_L(z)) z^{-2}} = \frac{B(z)}{A(z)}$$

Reflection function at the lips:

$$R_L(z) = \frac{B_L(z)}{A_L(z)} = -\frac{(b_L)_0 + (b_L)_1 z^{-1}}{(a_L)_0 + (a_L)_1 z^{-1}}$$

Amplitude-complementary transmission:

$$T_L(z) = 1 + R_L(z) = \frac{A_L(z) + B_L(z)}{A_L(z)}$$

Transfer function 3: frequency-dependent lip reflection:

$$\hat{H}_L(z) = \frac{(A_L(z) + B_L(z)) z^{-(N+1)} \prod_{m=1}^N (1 + k_m)}{K_{1,1} A_L(z) + K_{1,2} B_L(z) - R_0 (K_{2,1} A_L(z) + K_{2,2} B_L(z)) z^{-2}} = \frac{\hat{B}(z)}{\hat{A}(z)}$$

Transfer Function 3: numerator polynomial

Transfer function 3:
$$\hat{H}_L(z) = \frac{(A_L(z) + B_L(z))z^{-(N+1)} \prod_{m=1}^N (1 + k_m)}{K_{1,1}A_L(z) + K_{1,2}B_L(z) - R_0 (K_{2,1}A_L(z) + K_{2,2}B_L(z)) z^{-2}} = \frac{\hat{B}(z)}{\hat{A}(z)}$$

Consider the sum of polynomials in the numerator:

$$\begin{aligned} A_L(z) + B_L(z) &= 1 - (b_L)_0 + \underbrace{((a_L)_1 - (b_L)_1)}_{-(1 - (b_L)_0)} z^{-1} \\ &= (1 - (b_L)_0) \underbrace{(1 - z^{-1})}_{\text{simple first order high-pass filter}} \end{aligned}$$

shelf filter: when $0 < g_\pi < 1$

$$\cancel{(a_L)_0}^1 - (b_L)_0 = -((a_L)_1 - (b_L)_1)$$

The numerator becomes:
$$\hat{B}(z) = \underbrace{g}_{\text{gain}} \underbrace{(1 - z^{-1})}_{\text{pure delay}} z^{-(N+1)}$$

gain:
$$g = (1 - (b_L)_0) \prod_{m=1}^N (1 + k_M)$$

Transfer Function 3: denominator polynomial

Transfer function (3):

$$\hat{H}_L(z) = \frac{(A_L(z) + B_L(z))z^{-(N+1)} \prod_{m=1}^N (1 + k_m)}{\underbrace{K_{1,1}A_L(z) + K_{1,2}B_L(z) - R_0 (K_{2,1}A_L(z) + K_{2,2}B_L(z)) z^{-2}}_{\hat{A}(z) = \hat{a}_0 z^{-0} + \hat{a}_1 z^{-1} + \dots + \hat{a}_{2N+3} z^{-2N+3}}} = \frac{\hat{B}(z)}{\hat{A}(z)}$$

Coefficient (column) vector:

$$\hat{\mathbf{A}}_N = \begin{bmatrix} \mathbf{c}_N & 0 & 0 & 0 \\ \cdot & \tilde{\mathbf{d}}_N & 0 & 0 \\ \cdot & \cdot & \mathbf{d}_N & 0 \\ \cdot & \cdot & \cdot & \tilde{\mathbf{c}}_N \\ 0 & \cdot & \cdot & \cdot \\ 0 & 0 & \cdot & \cdot \\ 0 & 0 & 0 & \cdot \\ 0 & 0 & 0 & 0 \end{bmatrix} \hat{\mathbf{R}}_0 + \begin{bmatrix} 0 & 0 & 0 & 0 \\ \mathbf{c}_N & 0 & 0 & 0 \\ \cdot & \tilde{\mathbf{d}}_N & 0 & 0 \\ \cdot & \cdot & \mathbf{d}_N & 0 \\ \cdot & \cdot & \cdot & \tilde{\mathbf{c}}_N \\ 0 & \cdot & \cdot & \cdot \\ 0 & 0 & \cdot & \cdot \\ 0 & 0 & 0 & \cdot \end{bmatrix} \hat{\mathbf{R}}_1 = \begin{bmatrix} \hat{a}_0 \\ \hat{a}_1 \\ \hat{a}_2 \\ \vdots \\ \hat{a}_{2N+3} \end{bmatrix} \neq \mathbf{A}_N = \begin{bmatrix} 1 \\ 0 \\ a_2 \\ \vdots \\ 0 \\ a_{2N} \\ 0 \\ R_0 \end{bmatrix}$$

$$\hat{\mathbf{R}}_{0,1} = [(a_L)_{0,1} \quad -(b_L)_{0,1} \quad -R_0(a_L)_{0,1} \quad R_0(b_L)_{0,1}]^T$$

Estimating Lip Reflection Coefficients $\hat{\mathbf{A}}_N$ (and LPC?)

First 4 elements of $\hat{\mathbf{A}}_N$:

$$\begin{bmatrix} \hat{a}_0 \\ \hat{a}_1 \\ \hat{a}_2 \\ \hat{a}_3 \end{bmatrix} = \begin{bmatrix} (a_L)_0 \cancel{c_0}^1 + & 0 & + & 0 \\ (a_L)_1 \cancel{c_1}^1 + & 0 & + & 0 \\ (a_L)_0 c_2 - & (b_L)_0 d_{2(N-1)} - & R_0(a_L)_0 d_0 \\ (a_L)_1 c_2 - & (b_L)_1 d_{2(N-1)} - & R_0(a_L)_1 d_0 \end{bmatrix}$$

Last 4 elements of $\hat{\mathbf{A}}_N$:

$$\begin{bmatrix} \hat{a}_{2N} \\ \hat{a}_{2N+1} \\ \hat{a}_{2N+2} \\ \hat{a}_{2N+3} \end{bmatrix} = \begin{bmatrix} -(b_L)_0 d_0 - & R_0(a_L)_0 d_{2(N-1)} + & R_0(b_L)_0 c_2 \\ -(b_L)_1 d_0 - & R_0(a_L)_1 d_{2(N-1)} + & R_0(b_L)_1 c_2 \\ 0 + & 0 + & R_0(b_L)_0 \cancel{c_0}^1 \\ 0 + & 0 + & R_0(b_L)_1 \cancel{c_1}^1 \end{bmatrix}$$

elimination: $\frac{\frac{\hat{a}_3}{\hat{a}_1} - \frac{\hat{a}_2}{\hat{a}_0}}{\frac{\hat{a}_{2N}}{\hat{a}_{2N+2}} - \frac{\hat{a}_{2N+1}}{\hat{a}_{2N+3}}} = \frac{(b_L)_0 (b_L)_1}{(\cancel{a_L})_1 \hat{a}_1} = D \quad \longrightarrow \quad (b_L)_0 = \frac{D \hat{a}_1}{(b_L)_1} \quad R_0 = -\frac{\hat{a}_{2N+3}}{(\hat{\mathbf{b}}_L)_2} = -\frac{\hat{a}_{2N+2}}{(\hat{\mathbf{b}}_L)_1}$

shelf filter: when $0 < g_\pi < 1$

$$(\cancel{a_L})_0^1 - (b_L)_0 = -((\cancel{a_L})_1^{\hat{a}_1} - (b_L)_1) \quad \longrightarrow \quad (b_L)_0 = 1 + \hat{a}_1 - (b_L)_1$$

quadratic equation: $(b_L)_1^2 - (1 + \hat{a}_1)(b_L)_1 + D \hat{a}_1 = 0 \quad \longrightarrow \quad (b_L)_1 = \frac{1 + \hat{a}_1}{2} \pm \sqrt{\left(\frac{1 + \hat{a}_1}{2}\right)^2 - D \hat{a}_1}$

Summary

- Relationship between piecewise cylindrical waveguide model and LPC using **three (3) transfer functions**:
 - ✓ 1. non-polynomial form (sufficient for frequency-domain implementation)
 - ✓ 2. polynomial in z , with **scalar** loss
 - ✓ 3. polynomial in z , with **frequency-dependent** loss
 - ✓ acoustically-informed cylindrical open-end reflection function at the lips (shelf filter)
 - ✓ estimation of loss coefficients from LPC coefficients
- An accurate estimation of boundary losses may improve (with glottal pulse)
 - ✓ inverse modeling
 - ✓ estimation of reflection coefficients and cross-sectional area functions from LPC
 - ✓ fitting to a waveguide model (real-time parametric synthesis)